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Self-propulsion of droplets by spatially-varying surface topography

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Under partial wetting conditions, making a substrate uniformly rougher enhances the wetting characteristics of the corresponding smooth substrate—hydrophilic systems become even more hydrophilic and hydrophobic systems even more hydrophobic. Here we show theoretically that spatial texturing of the substrate topography may lead to spontaneous propulsion of droplets. Individual droplets tend to be driven toward regions of maximal roughness for intrinsically hydrophilic systems and toward regions of minimal roughness for intrinsically hydrophobic systems. Spatial texturing can be achieved by patterning the substrate with sinusoidal wrinkles whose wavelength varies in one direction (inhomogeneous wrinkling) or lithographically etching a radial pattern of fractal (Koch curve) grooves on the substrate. Richer energy landscapes for droplet trajectories can be designed by combining texturing of spatial topography with chemical or material patterning of the substrate.

1 Introduction

Consider a liquid droplet partially wetting a solid substrate such as glass in contact with a gas such as air. Broadly speaking a substrate may wet easily (hydrophilic) or poorly (hydrophobic) depending on the nature of the substrate, the liquid and the gas. More specifically the three relevant interfacial surface tensions determine the contact angle made by the liquid-gas contact line meeting the plane of the substrate. The contact angle is less than 90° for hydrophilic systems and greater than 90° for hydrophobic systems. A totally wetting thin film corresponds to a vanishing contact angle and a complete spherical drop balanced at a point on the substrate corresponds to the superhydrophobic limit with a 180° contact angle.

Uniform surface roughness amplifies the basic wetting characteristics of the corresponding planar system. For hydrophilic/ hydrophobic systems the greater substrate area, for a given planar projection, available on the rough substrate makes the wetting more/less favorable and lowers/raises the contact angle. What about surfaces with spatially inhomogeneous properties? Although it is known theoretically and experimentally that variable chemical patterning¹ and Leidenfrost droplets contacting hot surfaces with asymmetric sawtooth patterns^{2,3} can lead to spontaneous propulsion of droplets, this paper shows theoretically that pure inhomogeneous spatial topography of the surface with no other variability is sufficient to drive droplet motion. Droplets are expected to spontaneously move around in the landscape of the surface topography maximizing or minimizing the roughness for naturally hydrophilic/hydrophobic systems respectively. Thus self-propelled droplets can be engineered to follow prescribed paths without external drive by appropriately

designing the surface topography. We also propose specific experimental geometries that could be engineered to observe this phenomenon.

In addition, one may also vary the chemical composition of the surface so that the intrinsic surface tensions are spatially dependent. The combination of chemical and surface topography offers a richer variety of potential structures to obtain desired flow patterns. The African beetle *Stenocara* fog-basks by tilting forward into the early morning fog-laden wind of the Namib desert and collecting micron-sized water droplets on the smooth hydrophilic peaks of its fused overwings (elytra).⁴ Once a sufficiently massive droplet is formed it rolls downhill against the wind to pool in textured waxy hydrophobic troughs and from there the drop flows to the beetle's mouth. Surface structures modeled on the *Stenocara* wings have been synthesized by creating hydrophilic patterns on superhydrophobic surfaces with water/2-propanol solutions of a polyelectrolyte.⁵

2 Method

The principle of driving liquid droplets *via* roughness gradients is simple. The free energy of a liquid droplet on a substrate on length scales well below the capillary length, where surface tension dominates over gravity, is $F = -IA_c + \sigma_{SV}A_t + \sigma_{LV}A_{LV}$, where $I = \sigma_{SV} - \sigma_{SL}$ is the imbibition parameter,⁶ σ_{SL} , σ_{SV} and σ_{LV} are the respective surface tensions between the three phases (Solid/Liquid/Vapor). For water under 1 atm and at room temperature, $\sigma_{LV} = 72$ mN m⁻¹. For water on substrates made of molecular crystals or plastics, $\sigma_{SV} \approx 10-50$ mN m⁻¹ and $\sigma_{SL} = \sigma_{SO} - \sigma_{LV}$ by Young's relation.⁶ A_c is the contact area between the droplet and substrate, A_t is the (constant) total area of a substrate and A_{LV} is the area of the liquid–vapor interface, which is taken to be constant even when a droplet moves. The

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system of a liquid droplet on a rough substrate may also be viewed as a droplet on a flat substrate with an effective imbibition parameter I_{eff} resulting from the roughness. I_{eff} is defined by $IA_c \equiv I_{\text{eff}}A_0$, where A_0 is the planar projection of the actual contact area. For rough surfaces, $A_c > A_0$, as shown in Fig. 1(a), and therefore $I_{\text{eff}}/I > 1$. Up to irrelevant constants, the free energy of a droplet on a rough substrate is

$$F = -I_{\text{eff}}(\vec{x})A_0,\tag{1}$$

where $I_{\rm eff}$ varies from place to place when the spatial roughness is inhomogeneous. The wetting characteristics of a substrate/liquid composite system determine the sign of I and therefore I_{eff} . A hydrophilic system is characterized by I > 0 and an acute contact angle $\theta = \arccos(I/\sigma_{I,V})$. A hydrophobic system is characterized by I < 0 and an obtuse contact angle.⁶ When I, and so I_{eff} , is positive (negative) a substrate lowers (increases) its free energy when covered by a liquid. This spontaneously drives droplets on (hydrophobic) substrates towards rougher hvdrophilic (smoother) regions respectively. Eqn (1) can also be used to understand the movement of droplets on a chemically heterogeneous substrate where $I_{eff}(\vec{x})$ depends on the wetting characteristics of the chemical composition at the corresponding position on the substrate. Chemical methods that drive droplets by directly modifying the physical imbibition parameter are known.¹ Here we propose that liquid droplets will spontaneously move on substrates with suitable spatially varying topography alone, with no change in the physical imbibition parameter.

The self-propulsion of liquid droplets on substrates with inhomogeneous roughness can also be understood in terms of the uneven distribution of the Laplace pressure across the droplet. The contact angle for a rough substrate (θ_r) is given by $\cos\theta_r = r\cos\theta$, with $r = A_c/A_0$.⁷ Thus surface roughness amplifies the intrinsic wetting properties of the corresponding planar substrate. Take a droplet spanning a hydrophilic surface that is rougher on the left than on the right, as illustrated in Fig. 1(b). The contact angle is then smaller on the left than on the right: $\theta_A < \theta_B$. The mean curvature *H* at the B end thus exceeds that at the A end, leading to a Laplace over-pressure ($P = 2\sigma_{LV}H$) gradient from right to left driving the droplet to the rougher part of the surface. The reverse argument applies to a hydrophobic substrate, leading to motion towards the smoother part of the substrate. The self-propulsion of a droplet on a substrate

3 Results and discussion

To be specific, consider a droplet on a uniaxial sinusoidal substrate, as shown in Fig. 2(a), experimentally realizable *via* wrinkled membranes.⁸ The height of the substrate is represented by $z(x) = a_k \cos(kx)$, with translational invariance along the *y*-direction. The roughness amplitude a_k will be much smaller than the maximum height of the droplet so that the shape of the liquid-air interface is unaffected by the shape of the substrate. For small amplitude roughness, liquid droplets can be in complete contact with the substrate, since air pockets do not form underneath the liquid.^{6,7} The effective imbibition parameter is given by

$$\frac{I_{\rm eff}}{I} = \frac{4}{\pi} \int_0^1 dy \sqrt{1 - y^2} \sqrt{1 + \Gamma \sin^2(\tilde{k}y)},$$
(2)

where $\tilde{k} = kR$ is the dimensionless wavenumber and $\Gamma = a_k^2 k^2$. Clearly Γ , arising from the gradient of the substrate height, is the parameter controlling the effective imbibition. For $R \gg \frac{2\pi}{k}$, eqn (2) simplifies to⁹

$$\frac{I_{\rm eff}}{I} = \frac{2}{\pi} R(\Gamma), \tag{3}$$

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where $R(x) = \int_0^{\pi/2} d\theta \sqrt{1 + x \sin^2 \theta}$. In this limit the effective imbibition parameter is dependent only on the product of the amplitude and the wavenumber of the sinusoidal substrate. Fig. 3 is a numerical plot of the monotonic growth of $I_{\text{eff}}/I vs$. Γ . I_{eff}/I is doubled for $\Gamma \approx 8$. A simple gradient of the effective imbibition parameter over the substrate can be achieved by varying the wavenumber k along the groove axis (y), as shown in the schematic Fig. 2(b). Droplets are expected to migrate to maximize/ minimize the contact area for intrinsically hydrophilic/hydrophobic substrates. The magnitude of the driving force along the groove axis is proportional to the gradient of the effective imbibition parameter:



Fig. 2 (a) A liquid droplet partially wetting a substrate with a uniaxial sinusoidally modulated roughness. (b) Schematic plot of sinusoidal grooves with wavenumber monotonically increasing in the direction orthogonal to the sinusoidal height profile.







Fig. 3 The ratio of the effective imbibition parameter to the physical imbibition parameter versus $\Gamma = a_k^2 k^2$ for a liquid droplet partially wetting a sinusoidally modulated substrate.

$$\nabla_{y}I_{\text{eff}} = \frac{2I}{\pi} \left[R(\Gamma) - S(\Gamma) \right] \quad \frac{d\ln \tilde{k}(y)}{dy}, \tag{4}$$

where $S(x) = \int_0^{\pi/2} \frac{d\theta}{\sqrt{1 + x \sin^2 \theta}}$, and $R(x) - S(x) = \frac{\pi x}{4} - \frac{3\pi x^2}{32} + \mathcal{O}(x^3)$. The driving force thus

depends rather weakly on k(v) and vanishes as Γ tends to zero.

Rough substrates may also be designed based on fractals.¹⁰ Consider a substrate with etched grooves whose cross section is the lower half of the Koch curve, as illustrated in Fig. 4.11 The Koch curve may be constructed by starting with an equilateral triangle of side length a_0 and perimeter $L_0 = 3a_0$, then recursively adding equilateral triangles symmetrically on each line segment. After *n* steps, the perimeter of the new graph becomes $L_n = L_0(4/3)^n$ with the length of each elementary line segment being $a_n = a_0(1/3)^n$. The Hausdorff, or self-similarity, dimension of the Koch curve is $d_{\rm H} = 1n4/1n3 \approx 1.26^{.12}$ The order of a physically realizable Koch curve has an upper limit $n_{\text{max}} = \frac{\ln(a_0/a_n)}{\ln 3} \sim 8$ by specifying $a_n \sim 10$ nm and $a_0 \sim 0.1$ mm.¹³ Now consider a set of close-packed evenly aligned straight grooves constructed from an *n*-th order Koch curve. The distance between two neighboring grooves is twice the breadth of a groove. The contact area between a droplet of radius R and the fractal substrate, in the limit R much bigger than the breadth of a groove, is $A_c = \pi R^2 [1 + q(n)]$, where q(n = 0) = 3/4 and $q(n > 0) = 2(4/3)^{n-2} - 1/2$. Since q(n) is always positive, $A_c/A_0 > 1$. The effective imbibition parameter is

$$\frac{I_{\rm eff}}{I} = 1 + q(n). \tag{5}$$

Thus the effective imbibition parameter depends only on the order of the Koch curve n and is independent of the seed side



Fig. 4 A substrate etched by fractal grooves. The cross-sectional shape of the grooves is the lower half of the Koch curve, as shown in the inset.

length a_0 . I_{eff}/I is two for n = 1 and exceeds 10 for n = 8. Note that the extra volume of liquid inside the finer structure of the fractal grooves is negligible in the limit of large *n* as the area A_n of the *n*-th order Koch curve converges: $\lim_{n\to\infty} A_n = 2\sqrt{3}a_0^2/5 \sim a_0^2 \ll a_0 h$, where h is the droplet thickness.

An effective roughness gradient can be made by etching a radial array of grooves with Koch cross-section, as sketched in Fig. 4. We take an intrinsically hydrophobic surface inclined at an angle α to the horizontal. A droplet sitting near the origin (O) of the radial array is expected to move upward to reduce the contact energy provided that the gradient of the effective imbibition parameter is sufficient to overcome gravity. The number of grooves covered by a droplet of size R is $N = 2R/(L\delta\theta)$, where $\delta\theta$ is the angular distance between neighboring grooves and L is the distance of the droplet from the origin. For simplicity, consider the "far-field" limit in which the droplet is sufficiently far from the origin that all the grooves under the droplet are effectively parallel. The change in contact area due to the roughness is $\Delta A = A_{\rm c} - A_0 = \frac{1}{2} N \pi (b_n - l_0) R$, where b_n is the area of

a groove of unit length with $b_n(n>0) = \frac{3a_0}{2} \left(\frac{4}{3}\right)^n$ and $b_n(n=0) =$ $5a_0/3$, and $l_0 = 2a_0/3$ is the groove breadth. This results in an effective imbibition parameter

$$\frac{I_{\rm eff}}{I} = 1 + \frac{b_n - l_0}{L\delta\theta}.$$
 (6)

A droplet rising up a distance δL increases its gravitational potential energy by $\delta W = mg\delta L\sin\alpha$, where $m \sim \rho R^2 h$ is the mass of the droplet. Meanwhile the surface energy decreases by $\delta F =$ $A_0 \delta I_{\text{eff}}$, where $\delta I_{\text{eff}} = I_{\text{eff}}(L + \delta L) - I_{\text{eff}}(L)$. A spontaneous climb therefore requires $\delta I_{\text{eff}}/\delta L > mg \sin \alpha / A_0$. Inserting eqn (6) for the effective imbibition parameter yields

$$\frac{b_n - l_0}{l_0} > \frac{L^2 \,\delta\theta \,mg \sin\alpha}{A_0 I l_0}.\tag{7}$$

This condition can be satisfied for large droplets near the origin on substrates with dense grooves. The right hand side of eqn (7) is of the order $10\sin\alpha$ for $L \sim \text{cm}$, $R \sim \text{mm}$, $I \sim \text{mN} \text{ m}^{-1}$, $\delta\theta \sim a_0/L$ and $h \sim 0.1R$. Since $(b_n - l_0)/l_0 \sim 10$ for n = 5, radially carved grooves made of the 5-th order Koch curves would generate a sufficient roughness gradient to drive droplets uphill.

There are several points in our analysis that may ultimately call for a more thorough treatment. Sharp substrate edges impede the motion of droplets via pinning of the triple line.¹⁴ Adhesion hysteresis may also arise from the microscopic interactions between a droplet and the substrate.¹⁵ These two effects are the main source of frictional energy dissipation.¹⁶ We have neglected entirely viscous dissipation due to internal fluid flow within moving droplets.^{6,17} The contact angle hysteresis may also impede the motion of a droplet on a rough hydrophilic surface, while the contact angle hysteresis is greatly suppressed on a rough hydrophobic surface due to strong thermal fluctuations at the liquid-solid interface on the nanoscale.18 In addition, in response to the roughness gradient of a substrate, the originally circular contact profile of a liquid droplet may distort towards the more wettable region to reduce the contact energy.

4 Conclusion

The geometry-driven propulsion of droplets in a system with axial symmetry is found in both nature and the lab either in a tapered tube or along a spider silk fiber with a conic spindle-knots structure.^{19,20} In this paper, we show theoretically that liquid droplets on substrates can be driven by pure inhomogeneous spatial topography. The size of a droplet is required to be smaller than the capillary length such that gravity can be ignored, but big enough to sense the gradient of roughness. In addition to chemical, electrical and thermal methods, the geometric patterning method provides a new way of controlling droplet flow on substrates which we expect to find application in a variety of areas of wetting research.

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